

# Morphology-based non-rigid registration of coronary computed tomography and intravascular images through virtual catheter path optimization

Karim Kadry, Max L. Olender, Andreas Schuh, Abhishek Karmakar, Kersten Petersen, Michiel Schaap, David Marlevi, Adam UpdePac, Takuya Mizukami, Charles Taylor, Elazer R. Edelman, and Farhad R. Nezami

**Abstract**—Coronary computed tomography angiography (CCTA) provides 3D information on obstructive coronary artery disease, but cannot fully visualize high-resolution features within the vessel wall. Intravascular imaging, in contrast, can spatially resolve atherosclerotic in cross sectional slices, but is limited in capturing 3D relationships between each slice. Co-registering CCTA and intravascular images enables a variety of clinical research applications but is time consuming and user-dependent. This is due to intravascular images suffering from non-rigid distortions arising from irregularities in the imaging catheter path. To address these issues, we present a morphology-based framework for the rigid and non-rigid matching of intravascular images to CCTA images. To do this, we find the optimal virtual catheter path that samples the coronary artery in CCTA image space to recapitulate the coronary artery morphology observed in the intravascular image. We validate our framework on a multi-center cohort of 40 patients using bifurcation landmarks as ground truth for longitudinal and rotational registration. Our registration approach significantly outperforms other approaches for bifurcation alignment. By providing a differentiable framework for multi-modal vascular co-registration, our framework reduces the manual effort required to conduct large-scale multi-modal clinical studies and enables the development of machine learning-based co-registration approaches.

This work was partially supported by the National Institute of Health (1R01HL161069) to ERE and FRN and Heartflow, Inc.

KK, MLO, ERE are with the Institute of Medical Engineering, Massachusetts Institute of Technology, Cambridge, MA, USA (emails: kkadry@mit.edu, molender@mit.edu, ere@mit.edu)

AS, KP, MS, AU, and CT are with HeartFlow, Inc., Redwood City, CA, 94063, USA (emails: aschuh@heartflow.com, kpetersen@heartflow.com, mschaap@heartflow.com, aupdepac@heartflow.com, ctaylor@heartflow.com)

AK is with the Meinig School of Biomedical Engineering, Cornell University, Ithaca, NY 14850 (email: ak944@cornell.edu)

DM is with the Department of Molecular Medicine and Surgery, Karolinska Institute, Stockholm, Sweden, (email: david.marlevi@ki.se)

TM is with the Cardiovascular Center in Aalst, OLV Clinic,

Aalst, Belgium, (email: takuyamizukami@coreaalst.com) 46

FRN is with the Department of Surgery Brigham and Women's Hospital Harvard Medical School Boston, MA 02115, (email: frikhtegarnezami@bwh.harvard.edu) 47

**Index Terms**—Slice-to-volume registration, Image registration, free-form deformation, spatial transforms, optical coherence tomography, multi-modal data fusion. 48

## I. INTRODUCTION 49

Coronary computed tomography angiography (CCTA) is a 3D imaging modality that allows for the detection of stenotic atherosclerotic lesions and assists clinicians in the diagnosis and treatment of coronary artery disease (CAD). In contrast to the current gold standard of digital subtraction angiography (DSA), CCTA can be used to create 3D computational models of coronary blood flow that can estimate fractional flow reserve (FFR-CT), [1]. CCTA also provides information on soft-tissue intraplaque components within the wall, albeit with some limitations. For example, CCTA suffers from blooming artifacts in the presence of highly attenuating calcium deposits [2], [3], which, combined with comparably low image resolution, creates difficulties in resolving highly calcified arteries. In contrast, catheter based imaging modalities such as intravascular ultrasound (IVUS) and optical coherence tomography (OCT), provide high-fidelity cross-sectional images of the lumen and intra-plaque. However, catheter based modalities do not contain information on the 3D pose (location and orientation) for each frame, making it difficult to reconstruct the artery in 3D. Recovering the pose of each intravascular frame within the CCTA image is known as co-registration, and enables three key clinical applications. First, intravascular image slices can be directly used as ground-truth in clinical studies to study the viability of CCTA in assessing CAD-related diagnostic metrics such as luminal area [1], calcium morphology [4], and plaque burden [5]–[7]. Second, co-registration enables the creation of matched multi-modal datasets, which can be used to train neural networks for the segmentation of lumen and plaque within CCTA images. Third, high-fidelity segmentations derived from intravascular images can be used in tandem with the recovered poses to create high fidelity coronary digital twins [8]–[10]. Such patient-specific models enable the physics 50

based simulation of various biophysical phenomena such as hemodynamics [1], biomechanical pressurization [8], [9], and virtual interventions [11], [12], which guides clinical decision making and pathophysiological research.

Manual co-registration of CCTA and intravascular images is however, a challenging and time consuming task. Typically, cross-sectional frames of interest are extracted from the CCTA images which then have to be matched with corresponding frames from a catheter-based intravascular acquisition [1], [4], [5], [7]. Rigid registration in the longitudinal and rotational directions is usually achieved by matching single landmarks in both modalities, such as large bifurcations [4]. However, the beating of the heart, the irregular motion of the imaging catheter, and the rotation of the catheter about its own axis create non-rigid distortions that accumulate along the length of the pullback [13]. Manually correcting for such artifacts is prohibitively time-consuming, requiring a cardiologist to mark multiple fiducial points in both images and locate the equivalent frames accordingly. There is therefore a need for computational algorithms that non-rigidly register CCTA images to corresponding intravascular data in an automatic fashion.

Automatic co-registration techniques for longitudinal alignment typically consist of discretely optimizing a cost function over a set of longitudinal or rotational image shifts, where the cost function varies depending on the modalities being registered. Some proposed cost functions include metrics such as lumen diameters [14], lumen contours [15], [16], calcium thickness [15], [17], and image pixel intensities [13]. In addition to longitudinal co-registration, our prior work includes rigid rotational registration for intravascular pullbacks based on extracted features such as luminal contours [16]. However, the registration accuracy of all rigid registration methods is compromised by inconsistent motor pullback speeds, rotational drift, and cardiac motion, as these introduce non-rigid longitudinal and rotational distortions that misalign image features such as diseased plaque and bifurcations.

To compensate for the longitudinal, rotational, and transverse motion of the catheter, several non-rigid registration approaches have been proposed. Non-rigid registration of intravascular imaging datasets has been predominantly performed through dynamic time warping (DTW) and dynamic programming (DP) [13], [15], [18]. However, DTW introduces non-physiological assumptions into the registration process by discretely skipping or repeating intravascular frames, assumed to be evenly spaced along the longitudinal direction. In contrast to discrete approaches, previous works, including our own, have leveraged continuous non-rigid registration methods to model the longitudinal stretch and rotational drift between intravascular imaging frames using affine transforms and spline interpolation [1], [19]. While such continuous non-rigid methods are more realistic, they extensively rely on manual pre-processing and the annotation of all bifurcation zones for image registration and do not account for the bending of the catheter away from the vessel centerline.

Further, there has been an increasing interest in machine learning approaches to image co-registration in which a neural network is trained to predict a spatial transform that maps

a moving image onto a static target image [20]–[22]. Such approaches critically rely on differentiable spatial transforms and rendering operations for the back-propagation of gradients to adjust the neural network weights [23], [24]. While such transforms are available for co-registration of 3D medical images in rectangular coordinates [20], a similar framework that accounts for the unique variation in intravascular catheter motion has yet to be developed.

Given the previous limitations in prior approaches, we here propose a novel slices-to-volume registration framework that aligns a set of intravascular image slices to their equivalent location in a volumetric CCTA image. The proposed continuous registration methodology does not require manual matching of morphological landmarks, requires only the morphology (lumen and vessel wall) for both modalities, along with the centerline within the CCTA image space. Specifically, we explore the problem of reconstructing the path of a *virtual catheter* sampling from a 3D CCTA-derived lumen morphology such that the cross sectional slices sampled by the virtual catheter match the image slices from the equivalent intravascular pullback. We specifically demonstrate our algorithm in the case of OCT intravascular pullbacks, where our key contributions are as follows:

- We introduce a differentiable and non-rigid spatial transform that acts on a set of frames defining the path of a virtual catheter in 3D space. The transform is formulated in terms of intravascular catheter motion, specifically modelling longitudinal, rotational, and transverse distortions. Our spatial transform is regularized to enforce priors regarding cumulative motion distortions and smoothness, while also being compatible with deep learning registration frameworks.
- We propose a rigid and non-rigid registration procedure for intravascular image slices and CCTA volumes, based on matching lumen and vessel wall morphology between modalities. The virtual catheter is initialized by the rigid registration step and then stretched, twisted, and bent by the non-rigid step through gradient-based optimization. For non-rigid registration, we choose to optimize the similarity between luminal distance fields and introduce several pre-processing steps to stabilize the process.
- We demonstrate the capabilities of our registration procedure on a multi-center dataset of 40 CCTA and OCT images with manually annotated landmarks. We directly benchmark against our previously developed discrete optimization approach and demonstrate improved registration error.

## II. METHODOLOGY

An overview of the co-registration pipeline is detailed in Fig. 1. In brief, our registration algorithm II-A takes as input morphological representations of lumen and vessel wall for the CCTA and intravascular images, in addition to the CCTA lumen centerline. In this study, we utilize OCT pullbacks as our intravascular imaging modality. For rigid registration, a virtual catheter is first initialized from the centerline in the form of 3D frame positions and poses detailing the

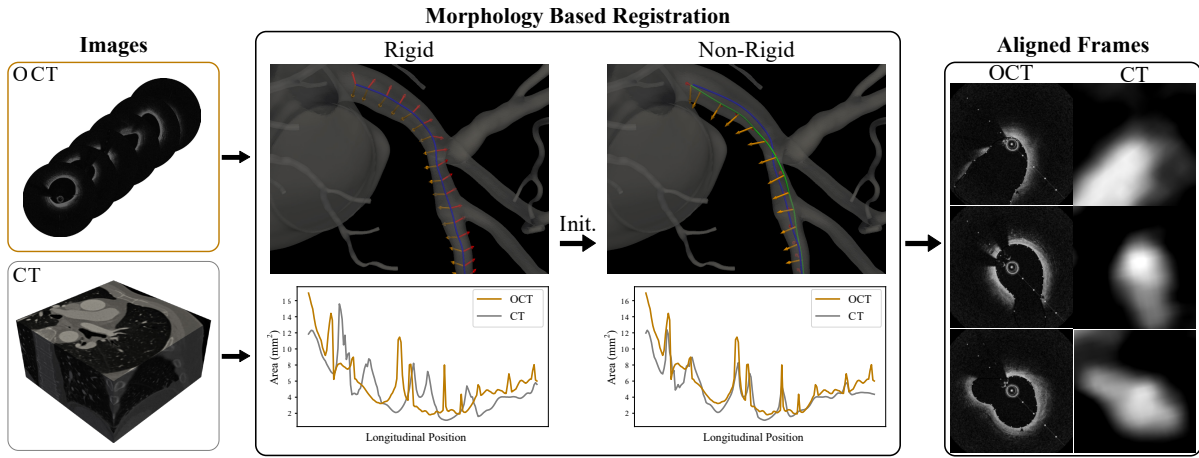


Fig. 1. Overview of the proposed registration pipeline. Lumen and vessel wall morphologies are derived from OCT and CCTA images and given as input to the registration process along with an initial centerline centerline in CCTA space. A rigid co-registration step initializes the virtual catheter path (blue), where the pose of each frame is described by orientation vectors (red and orange arrows). The virtual catheter path is used to sample a virtual pullback of the CCTA morphology in the form of a luminal distance field. The morphological similarity between the OCT and CCTA pullbacks is used to guide the non-rigid registration step. The alignment process stretches, twists, and bends the virtual catheter frames to produce an aligned catheter path (green) that can sample equivalent CCTA frames for each intravascular image slice.

orientation of each frame. These frames are used to sample cross sections from the CCTA morphology to produce a virtual pullback (section II-A.2). The sampled pullback is used for longitudinal and rotational alignment (section II-A.3), which outputs crop indices and a rotation angle that initialize the non-rigid registration process. Non-rigid registration (section II-A.4) optimizes a spatial transform applied to the virtual catheter that aligns the morphology between the virtual and intravascular pullbacks. The non-rigid spatial transformation consists of longitudinal (section II-A.6), rotational (section II-A.7), and transverse (section II-A.8) deformation steps. To evaluate our method, we use morphological representations derived from a multi-center clinical image dataset and evaluate the performance of our algorithm against discrete optimization baselines (section II-B).

### A. Co-registration framework

1) *Input morphological representations*: As CCTA and intravascular images are dissimilar in their image characteristics, we choose to align the images based on morphological representations of the lumen and vessel wall. The four input morphologies consist of the luminal Signed Distance Fields (SDFs) ( $\mathbf{L}_{CT}^{3D}$ ,  $\mathbf{L}_{OCT}^{pull}$ ), as well as the vessel wall SDFs ( $\mathbf{W}_{CT}^{3D}$ ,  $\mathbf{W}_{OCT}^{pull}$ ) for both modalities. The superscripts '3D' and 'pull' indicate whether the SDF is located in 3D cartesian space or the cylindrical space defined by the catheter respectively.

2) *Virtual catheterization*: To compare both modalities in the same coordinate system, we leverage curved-planar reformation [25], where a virtual catheter samples cross-sectional slices from the CCTA lumen and vessel wall to produce  $\mathbf{L}_{CT}^{pull}$  and  $\mathbf{W}_{CT}^{pull}$  respectively. The virtual catheter is defined by a set of frames in 3D space that are constructed through a two step process that takes as input the set of  $n$  CCTA centerline

points  $\mathbf{R} \in \mathbb{R}^{n \times 3}$  arranged in 3D space. The first step consists of finding the set of tangent vectors  $\mathbf{T} \in \mathbb{R}^{n \times 3}$  by applying a spatial derivative on  $\mathbf{R}$ , defining normal vectors for each frame. The second step consists of finding the orthogonal orientation vectors  $\mathbf{U} \in \mathbb{R}^{n \times 3}$  and  $\mathbf{V} \in \mathbb{R}^{n \times 3}$  that define the angular orientation of each frame. This is done through randomly initializing the orthogonal vectors for the first frame and applying parallel transport [26] along the centerline, which ensures that all orientation vectors remain stable between frames. The frames  $\mathbf{F} \in \mathbb{R}^{n \times 3 \times 4}$  are finally obtained by concatenating the position and orientation vectors,

$$\mathbf{F} = \text{concat}(\mathbf{R}, \mathbf{T}, \mathbf{U}, \mathbf{V}). \quad (1)$$

To produce a virtual pullback, the frame matrix  $\mathbf{F}$  is represented as a set of planar pointclouds and is used to sample the CCTA SDFs ( $\mathbf{L}_{CT}^{3D}$ ,  $\mathbf{W}_{CT}^{3D}$ ) for each point, where the cross-sectional size of the resulting grid matches that of the intravascular dataset,

$$\mathbf{L}_{CT}^{pull} = \text{VirtualCatheter}(\mathbf{F}, \mathbf{L}_{CT}^{3D}), \quad (2)$$

$$\mathbf{W}_{CT}^{pull} = \text{VirtualCatheter}(\mathbf{F}, \mathbf{W}_{CT}^{3D}). \quad (3)$$

3) *Rigid registration*: An overview of the rigid registration step can be seen in Fig. 2 and Algorithm 1. We first construct the virtual catheter frames  $\mathbf{F}^{ori}$  from the input centerline points  $\mathbf{R}_{ori}$  and use them to initialize the virtual pullbacks  $\mathbf{L}_{CT}^{pull}$  and  $\mathbf{W}_{CT}^{pull}$ , which are used for longitudinal and rotational registration respectively. For the rigid longitudinal registration, we binarize the luminal SDFs ( $\mathbf{L}_{CT}^{pull}$  &  $\mathbf{L}_{OCT}^{pull}$ ) and create area vectors for each modality. We leverage our previous work to rigidly align the pullbacks using a multi-step sliding window method, minimizing the difference in area vectors and bifurcation locations [16]. The resulting output consists of

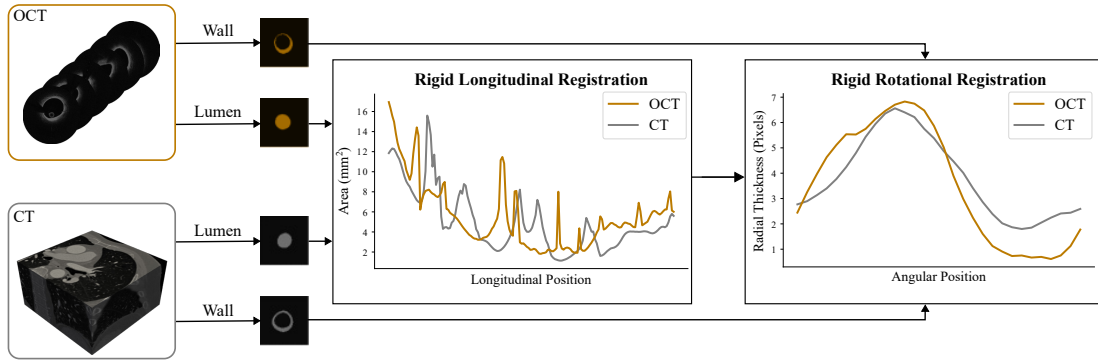


Fig. 2. Overview of the proposed rigid registration pipeline. Lumen area vectors from both modalities are used for rigid registration in the longitudinal direction using a sliding window approach. The longitudinal registration is used to crop each segmentation such that they have the same starting point for rotational registration. The vessel wall segmentations for all frames are converted to vessel thickness-angle plots and are used to determine a single optimal rotation for the entire pullback.

### Algorithm 1 Full Co-registration Algorithm

**Require:**  $\mathbf{R}^{\text{ori}}$   $\triangleright$  CCTA Original Centerline Points

**Require:**  $\mathbf{L}_{\text{CT}}^{\text{3D}}, \mathbf{L}_{\text{OCT}}^{\text{pull}}$   $\triangleright$  luminal Signed Distance Fields

**Require:**  $\mathbf{W}_{\text{CT}}^{\text{3D}}, \mathbf{W}_{\text{OCT}}^{\text{pull}}$   $\triangleright$  Wall Signed Distance Fields

#### Initialize Pullback from CCTA Morphology (Sec. II-A.2)

1:  $\mathbf{F}^{\text{ori}} \leftarrow \text{InitFrames}(\mathbf{R}^{\text{ori}})$   $\triangleright$  Frame Positions & Poses

2:  $\mathbf{L}_{\text{CT}}^{\text{pull}} \leftarrow \text{VirtualCatheter}(\mathbf{F}^{\text{ori}}, \mathbf{L}_{\text{CT}}^{\text{3D}})$

3:  $\mathbf{W}_{\text{CT}}^{\text{pull}} \leftarrow \text{VirtualCatheter}(\mathbf{F}^{\text{ori}}, \mathbf{W}_{\text{CT}}^{\text{3D}})$

#### Rigid Registration w/ Lumen & Vessel Wall (Sec. II-A.3)

4:  $\mathbf{C} \leftarrow \text{LongReg}(\mathbf{L}_{\text{CT}}^{\text{pull}}, \mathbf{L}_{\text{OCT}}^{\text{pull}})$   $\triangleright$  Crop Indices

5:  $\vartheta \leftarrow \text{RotReg}(\mathbf{C}, \mathbf{W}_{\text{CT}}^{\text{pull}}, \mathbf{W}_{\text{OCT}}^{\text{pull}})$   $\triangleright$  Rotation Angle

#### Non-rigid Registration w/ Lumen (Sec. II-A.4)

6:  $\mathbf{F}_{\varphi} \leftarrow \text{NonrigidReg}(\mathbf{C}, \vartheta, \mathbf{F}^{\text{ori}}, \mathbf{L}_{\text{CT}}^{\text{3D}}, \mathbf{L}_{\text{OCT}}^{\text{pull}})$

7: **return**  $\mathbf{F}_{\varphi}$

cropping indices  $\mathbf{C} = \{\mathbf{C}_{\text{CT}}, \mathbf{C}_{\text{OCT}}\}$  determining the shared starting points for each modality.

$$\mathbf{C} = \text{LongReg}(\mathbf{L}_{\text{CT}}^{\text{pull}}, \mathbf{L}_{\text{OCT}}^{\text{pull}}), \quad (4)$$

For rigid rotational registration, using luminal profiles for rigid rotational alignment was deemed unreliable due to the CCTA-derived morphology being circularly symmetric. Therefore, we take as input the vessel wall SDFs ( $\mathbf{W}_{\text{CT}}^{\text{pull}}, \mathbf{W}_{\text{OCT}}^{\text{pull}}$ ) that were correspondingly binarized to produce segmentation maps. For both wall segmentations, a wall thickness matrix  $\mathbf{H} \in \mathbb{R}^{n \times \gamma}$  by tracing  $\gamma$  radial rays from the centroid of all  $n$  frames of the vessel segmentation in equally spaced circumferential increments. We crop the thickness matrices for the CCTA ( $\mathbf{H}_{\text{CT}}$ ) and OCT ( $\mathbf{H}_{\text{OCT}}$ ) images using the indices  $\mathbf{C}$  such that they are longitudinally aligned with the same starting points. The optimal rigid rotation angle  $\vartheta$  is obtained by circumferentially sliding one thickness matrix over the other and minimizing the mean squared error,

$$\vartheta = \text{RotReg}(\mathbf{W}_{\text{CT}}^{\text{pull}}, \mathbf{W}_{\text{OCT}}^{\text{pull}}). \quad (5)$$

4) *Non-rigid registration overview:* The non-rigid registration process can be seen in Fig. 3 and Algorithm 2. The input consists of the initialized frame variables  $\mathbf{F}^{\text{ori}}$ , cropping indices  $\mathbf{C}$ , rotation angle  $\vartheta$ , and the luminal SDFs ( $\mathbf{L}_{\text{CT}}^{\text{3D}}, \mathbf{L}_{\text{CT}}^{\text{pull}}$ ). We formulate the problem in terms of finding the set of frames  $\mathbf{F}^{\varphi}$  that correspond to the original path of the intravascular catheter in CCTA image space. This is done by maximizing the morphological similarity between the intravascular pullback and the CCTA virtual pullback sampled with spatially transformed frames  $\mathbf{F}^{\varphi}$ . First, the rigidly initialized frames  $\mathbf{F}$  are obtained by cropping and rotating the input frames  $\mathbf{F}^{\text{ori}}$  according to the outputs of rigid registration ( $\mathbf{C}, \vartheta$ ). The updated frame variables  $\mathbf{F}^{\varphi}$  are produced through three sequentially applied non-rigid spatial transforms  $\varphi_{\text{long}}, \varphi_{\text{rot}}$ , and  $\varphi_{\text{trans}}$  in the longitudinal, rotational, and transverse directions respectively:

$$\mathbf{F}^{\varphi} = \varphi_{\text{trans}} \circ \varphi_{\text{rot}} \circ \varphi_{\text{long}} \circ \mathbf{F}, \quad (6)$$

where  $\circ$  is the composition operator. The morphological similarity function was defined as the mean squared error between the CCTA morphology  $\mathbf{L}_{\text{CT}}^{\text{pull}}$  sampled with the spatially transformed frames  $\mathbf{F}^{\varphi}$  and the OCT morphology  $\mathbf{L}_{\text{OCT}}^{\text{pull}}$  that is considered as a target. We specifically clamp the SDFs to only have non-zero values inside the lumen to prevent the virtual catheter from switching to the incorrect coronary branch:

$$\mathcal{L} = \text{MSE}(\text{clamp}(\mathbf{L}_{\text{CT}}^{\text{pull}}), \text{clamp}(\mathbf{L}_{\text{OCT}}^{\text{pull}})). \quad (7)$$

This approach was used instead of a segmentation-based similarity function, such as cross-entropy or Dice, as binary-segmentation-based losses reach a minimum value when there is complete overlap between segmentations and thus are poor surrogates for alignment [27]. In contrast, distance field-based losses continue to change even after complete overlap is achieved, allowing for enhanced registration accuracy.

5) *Virtual Catheter Manipulation:* Instead of directly manipulating the 3D positions and orientations of the frames  $\mathbf{F}$  to produce  $\mathbf{F}^{\varphi}$ , each spatial transform takes as input one or more frame manipulation vectors that represent the stretching, twisting, and bending of the original virtual catheter path. As such, we define four frame manipulation vectors ( $\mathbf{s}, \boldsymbol{\theta}, \mathbf{d}^u, \mathbf{d}^v$ ) representing 1) the arclength positions along the

virtual catheter path  $\mathbf{s}$ , 2) the rotation angles of each frame  $\theta$  about the catheter, and 3) the in-plane transverse displacements  $\mathbf{d}^u$  and  $\mathbf{d}^v$  (see Fig. 3). This parametrization enables us to regularize the virtual catheter path to be smooth along the pullback, with independent smoothness constraints for each deformation type. To enforce such constraints, we control the frame manipulation vectors through B-spline deformations [28] parametrized by a sparse set of control points.

---

**Algorithm 2** Non-rigid Co-registration
 

---

**Require:**  $\mathbf{C}, \vartheta, \mathbf{F}^{\text{ori}}$   $\triangleright$  Crop Indices, Rotation Angle, Frames

**Require:**  $\mathbf{L}_{\text{CT}}^{\text{3D}}, \mathbf{L}_{\text{OCT}}^{\text{pull}}$   $\triangleright$  Luminal Signed Distance Fields

- 1:  $\mathbf{s}_{\text{init}}, \theta_{\text{init}}, \mathbf{d}_{\text{init}}^u, \mathbf{d}_{\text{init}}^v \leftarrow \text{InitFrameVars}()$
- 2:  $\mathbf{p}^s, \mathbf{p}^\theta, \mathbf{p}^u, \mathbf{p}^v \leftarrow \text{InitCtrlPts}()$
- 3:  $\mathbf{x}^s, \mathbf{x}^\theta \leftarrow \text{InitRelVecs}()$   $\triangleright$  Stretch & Twist Vectors
- 4:  $\mathbf{F}, \mathbf{L}_{\text{OCT}}^{\text{pull}} \leftarrow \text{RigidInit}(\mathbf{C}, \vartheta, \mathbf{F}^{\text{ori}}, \mathbf{L}_{\text{OCT}}^{\text{pull}})$
- 5: **for**  $i \in \{1, \dots, \text{Epochs}\}$  **do**  $\triangleright$  Optimization Loop

---

**Stretch Frames (Sec. II-A.6)**


---

- 6:  $\mathbf{p}^s \leftarrow \text{DeformCtrlPts}(\mathbf{x}^s)$   $\triangleright$  Equation 10
- 7:  $\mathbf{s} \leftarrow \text{BsplineDeform}(\mathbf{s}_{\text{init}}, \mathbf{p}^s)$   $\triangleright$  Equation 9
- 8:  $\mathbf{F}^s \leftarrow \varphi_{\text{long}}(\mathbf{s}) \circ \mathbf{F}$ .  $\triangleright$  Equation 8

---

**Twist Frames (Sec. II-A.7)**


---

- 9:  $\mathbf{p}^\theta \leftarrow \text{DeformCtrlPts}(\mathbf{x}^\theta)$   $\triangleright$  Equation 13
- 10:  $\theta \leftarrow \text{BsplineDeform}(\theta_{\text{init}}, \mathbf{p}^\theta)$   $\triangleright$  Equation 12
- 11:  $\mathbf{F}^\theta \leftarrow \varphi_{\text{rot}}(\theta) \circ \mathbf{F}^s$   $\triangleright$  Equation 11

---

**Bend Frames (Sec. II-A.8)**


---

- 12:  $\mathbf{d}^u \leftarrow \text{BsplineDeform}(\mathbf{d}_{\text{init}}^u, \mathbf{p}^u)$   $\triangleright$  Equation 16
- 13:  $\mathbf{d}^v \leftarrow \text{BsplineDeform}(\mathbf{d}_{\text{init}}^v, \mathbf{p}^v)$   $\triangleright$  Equation 16
- 14:  $\mathbf{F}^\varphi \leftarrow \varphi_{\text{trans}}(\mathbf{d}^u, \mathbf{d}^v) \circ \mathbf{F}^\theta$   $\triangleright$  Equation 14

---

**Update Parameters**


---

- 15:  $\mathbf{L}_{\text{CT}}^{\text{pull}} \leftarrow \text{VirtualCatheter}(\mathbf{F}^\varphi, \mathbf{L}_{\text{CT}}^{\text{3D}})$
  - 16:  $\mathcal{L} \leftarrow \text{MSE}(\text{clamp}(\mathbf{L}_{\text{CT}}^{\text{pull}}), \text{clamp}(\mathbf{L}_{\text{OCT}}^{\text{pull}}))$   $\triangleright$  Loss
  - 17:  $\mathbf{x}^s, \mathbf{x}^\theta, \mathbf{p}^u, \mathbf{p}^v \leftarrow \text{Adam}(\nabla \mathcal{L})$   $\triangleright$  Backprop & Step
  - 18: **end for**
  - 19: **return**  $\mathbf{F}^\varphi$
- 

6) *Non-rigid longitudinal registration*: The spatial transform  $\varphi_{\text{long}}$  governing the inter-frame spacing along the virtual catheter takes in the arclength vector  $\mathbf{s}$  and resamples a spline based on the initial centerline points  $\mathbf{R}$  to produce an updated set of centerline coordinates  $\mathbf{R}^s$ . The frame poses ( $\mathbf{T}^s, \mathbf{U}^s$ , and  $\mathbf{V}^s$ ) are then recalculated and used to update the frame matrix:

$$\mathbf{F}^s = \varphi_{\text{long}}(\mathbf{s}) \circ \mathbf{F}. \quad (8)$$

The initial arclength vector  $\mathbf{s}_{\text{init}} \in \mathbb{R}^n$  is set to be monotonically increasing from 0 to 1, and is updated by a B-spline transform:

$$\mathbf{s} = \mathbf{B}^s \mathbf{p}^s, \quad (9)$$

in which  $\mathbf{s} \in \mathbb{R}^n, \mathbf{B}^s \in \mathbb{R}^{n \times m_s}, \mathbf{p}^s \in \mathbb{R}^{m_s}$  where  $n$  is the number of frames and  $m_s$  is the number of longitudinal control points.  $\mathbf{B}^s$  is the univariate B-spline tensor and is pre-computed from the initial arclength vector  $\mathbf{s}_{\text{init}}$ , while  $\mathbf{p}^s$  is the deformed control point vector that is initialized as a monotonically increasing vector of length  $m_s$ .

To account for the cumulative effect of catheter motor speed variation, we do not directly optimize the control points  $\mathbf{p}^s$ . Instead, we optimize for the relative stretch vector  $\mathbf{x}^s \in \mathbb{R}^{m_s-1}$  that determines the cumulative displacement of each control point  $\Delta p_i^s$ , with the most proximal control point remaining fixed,

$$\Delta p_j^s = x_j^s + \sum_{k=0}^{j-1} x_k^s. \quad (10)$$

To regularize the virtual catheter motion and prevent backward movement, the relative deformation of each control point  $\Delta p_j^s$  is limited to a fraction of the distance between the control points through clamping.

7) *Non-rigid rotational registration*: The rotational transform  $\varphi_{\text{rot}}$  is applied to the longitudinally adjusted frames  $\mathbf{F}^s$  and takes in the rotation angles  $\theta$  to produce the rotationally adjusted frames  $\mathbf{F}^\theta$ . This is done by rotating the longitudinally adjusted orientation vectors  $\mathbf{U}^s$  and  $\mathbf{V}^s$  about the tangent vector set  $\mathbf{T}^s$ .

$$\mathbf{F}^\theta = \varphi_{\text{rot}}(\theta) \circ \mathbf{F}^s \quad (11)$$

The initial rotation vector  $\theta_{\text{init}} \in \mathbb{R}^n$  is initialized with zeros and is updated by a B-spline transform:

$$\theta = \mathbf{B}^\theta \mathbf{p}^\theta, \quad (12)$$

where  $\theta \in \mathbb{R}^n, \mathbf{B}^\theta \in \mathbb{R}^{n \times m_\theta}, \mathbf{p}^\theta \in \mathbb{R}^{m_\theta}$ , where  $m_\theta$  is the number of control points and  $\mathbf{B}^\theta$  is a B-spline tensor that is pre-computed from the initial rotation vector  $\theta_{\text{init}}$ . The rotational control point vector  $\mathbf{p}^\theta$  is initialized as a zero vector and is updated similarly to the longitudinal control points, where the rotation defined for each control point is updated by a relative twist vector  $\mathbf{x}^\theta \in \mathbb{R}^{m_\theta-1}$ . The cumulative rotation value for each control point is therefore defined by:

$$\Delta p_j^\theta = x_j^\theta + \sum_{k=0}^{j-1} x_k^\theta, \quad (13)$$

8) *Non-rigid transverse registration*: The transverse transform  $\varphi_{\text{trans}}$  is applied to the rotationally adjusted frames  $\mathbf{F}^\theta$  and takes as input displacement magnitude vectors  $\mathbf{d}^u$  and  $\mathbf{d}^v$  to produce the final frames  $\mathbf{F}^\varphi$ . This is done by displacing the rotationally aligned centerline points  $\mathbf{R}^\theta$  along  $\mathbf{U}^\theta$  and  $\mathbf{V}^\theta$  to obtain  $\mathbf{R}^\varphi$ .

$$\mathbf{F}^\varphi = \varphi_{\text{trans}}(\mathbf{d}^u, \mathbf{d}^v) \circ \mathbf{F}^\theta \quad (14)$$

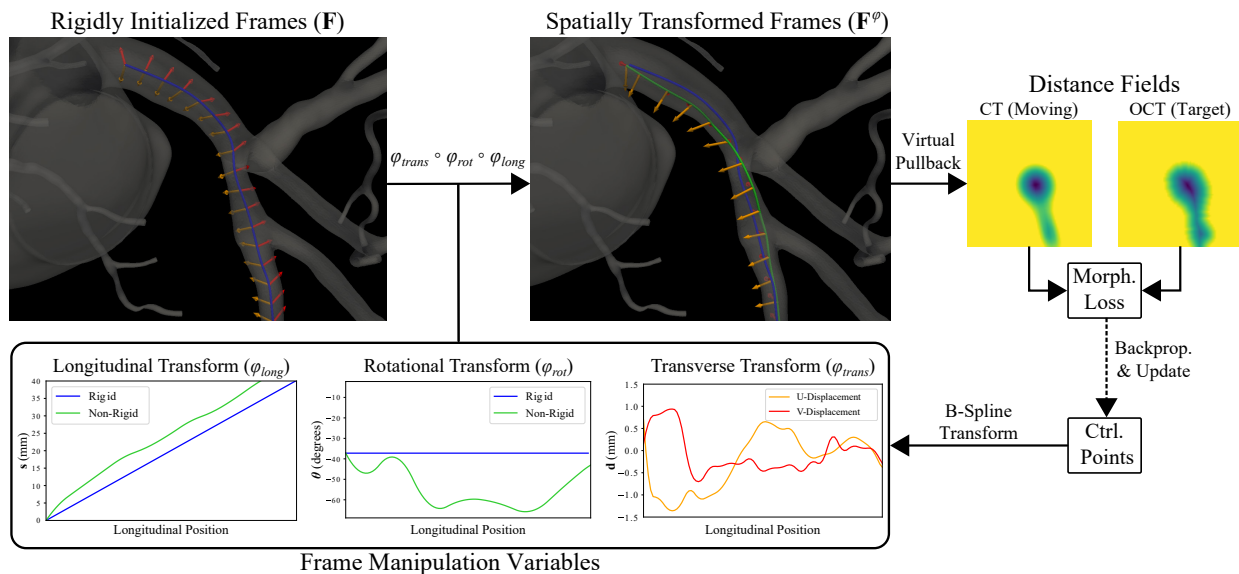
In contrast to the longitudinal and rotational transforms, the transverse transform  $\varphi_{\text{trans}}$  consists of two separate operations ( $\varphi_{\text{trans}}^u$  and  $\varphi_{\text{trans}}^v$ ) that control the transverse displacement of the catheter path away from the artery center in orthogonal directions.

$$\varphi_{\text{trans}}(\mathbf{d}^u, \mathbf{d}^v) = \varphi_{\text{trans}}^u(\mathbf{d}^u) \circ \varphi_{\text{trans}}^v(\mathbf{d}^v), \quad (15)$$

The initial in-plane transverse displacements  $\mathbf{d}^u$  and  $\mathbf{d}^v$  are initialized to be zero and are calculated by the following relation:

$$\mathbf{d}^u = \mathbf{B}^u \mathbf{p}^u. \quad \text{and} \quad \mathbf{d}^v = \mathbf{B}^v \mathbf{p}^v. \quad (16)$$

where each displacement vector is controlled by control points



**Fig. 3.** Overview of the spatial deformation acting on the rigidly initialized virtual catheter path represented by a frame matrix  $\mathbf{F}$ . The frames are acted upon by the longitudinal transform  $\varphi_{\text{long}}$  that stretches and compresses the space between adjacent frames according to the longitudinal position vector  $s$ . The rotational transform  $\varphi_{\text{rot}}$  rotates each orientation vector (red and orange arrows) about the catheter axis (blue line) according to the rotational vector  $\theta$ . The transverse transform  $\varphi_{\text{trans}}$  shifts the frame centers in the direction of the rotated orientation vectors according to transverse displacement vectors  $d^u$  and  $d^v$ . The spatially transformed frame matrix  $\mathbf{F}^\varphi$  is used to sample cross sections from the CCTA lumen morphology that are compared to the target morphology derived from the OCT lumen. The parameters controlling the spatial transforms are then updated with gradient descent.

381  $\mathbf{p}^u$  and  $\mathbf{p}^v$ . The virtual catheter is initialized to stay close  
 382 to the centerline by setting the two control point vectors as  
 383 zero-vectors of length  $m_d$  each. In contrast to longitudinal  
 384 and rotational registration, we directly optimize the control  
 385 points as the artery wall constrains the cumulative transverse  
 386 displacement of the catheter.

### 387 B. Evaluation

388 1) *Image data*: To evaluate our proposed co-registration  
 389 framework, a dataset consisting of 40 matched OCT and CCTA  
 390 image pairs from five different clinical centers were selected,  
 391 all originating from the Precise Percutaneous Coronary Inter-  
 392 vention Plan (P3) study [29]. As each OCT pullback image  
 393 consisted of 375 frames, the intravascular imaging dataset  
 394 comprised of approximately 15,000 image frames before ex-  
 395 cluding frames with poor image quality. The OCT lumen in  
 396 every frame was manually annotated by trained cardiologists,  
 397 and continuous segments of the OCT pullback with poor  
 398 lumen segmentations due to residual blood or catheter housing  
 399 were manually excluded. Further, as no manual annotations  
 400 were available, the vessel wall borders in every OCT frame  
 401 were segmented using a convolutional neural network through  
 402 a U-net architecture [30]. Details of the network, training,  
 403 and validation can be found in section II-B.5. The lumen and  
 404 vessel wall segmentations were re-sampled to represent a 3D  
 405 image of dimensions  $(96 \times 96 \times n)$  with an in-frame resolution  
 406 of 80 micrometers and an out-of-frame resolution of 0.4 mm  
 407 (sampling every other longitudinal frame). The segmentations  
 408 of the lumen and vessel wall were used to produce the SDFs  
 409  $\mathbf{L}_{\text{OCT}}^{\text{pull}}$  and  $\mathbf{W}_{\text{OCT}}^{\text{pull}}$  using the fast marching method [31]. All  
 410 utilized intravascular pullback sections were manually deemed  
 411 to sufficiently visualize the artery. For the CCTA data, a

387 3D surface mesh of the coronary tree for each patient was  
 388 provided by a previously validated virtual planner [32]. These  
 389 meshes were produced by a deep learning algorithm and  
 390 are minimally corrected through human annotators. The 3D  
 391 models are used to produce high-resolution SDFs of the lumen  
 392 and vessel wall  $\mathbf{L}_{\text{CT}}^{\text{3D}}$  and  $\mathbf{W}_{\text{CT}}^{\text{3D}}$  with a resolution of 0.25  
 393 mm along each axis and a shape of of  $(768 \times 768 \times 482)$ .  
 394

395 The CCTA SDFs were stored as truncated signed distance  
 396 fields, only containing positive distance values up to 2mm.  
 397 This was done to enable high-fidelity sampling through virtual  
 398 catheterization while also reducing the pre-processing cost.  
 399 The vessel centerlines were semi-automatically obtained by  
 400 annotating the start and end points of each artery and using  
 401 them as input to VMTK [33].  
 402

403 2) *Co-registration evaluation*: In order to evaluate the per-  
 404 formance of the non-rigid registration, 114 bifurcations were  
 405 manually marked by human experts in the OCT pullback  
 406 as well as in the rigid and non-rigid virtual pullback seg-  
 407 mentations generated from the CCTA data. Bifurcations were  
 408 defined as the last image frame before a coronary artery  
 409 splitting into two branches could be seen. The landmark  
 410 annotations were first annotated before non-rigid registration  
 411 for the rigidly aligned data belonging to both modalities.  
 Specifically, bifurcations that were common to both modalities  
 had their frame numbers recorded for validation of the non-  
 rigid registration algorithm. The initially annotated bifurca-  
 tions in the CCTA pullback were then re-annotated after non-  
 rigid registration. Longitudinal validation was conducted by  
 comparing the frame number of a bifurcation in the OCT data  
 with the equivalent bifurcation frame number in the virtual  
 pullback before and after non-rigid registration.  
 412

413 In order to validate the non-rigid rotational registration,  
 414  
 415

444 the manually annotated bifurcation angles for the OCT pull-  
 445 back and the virtual pullback were compared before and  
 446 after rotational registration. As the bifurcation angle between  
 447 bifurcation sections that were not longitudinally matched is  
 448 expected to be uncorrelated, only bifurcations that had a frame  
 449 mismatch below a certain number of frames were considered  
 450 for qualitative analysis of rotational accuracy. The longitudinal  
 451 mismatch threshold was chosen as double the kernel size of  
 452 the Gaussian filter applied to the SDF (six frames).

453 *3) Implementation details:* The rigid longitudinal registra-  
 454 tion parameters were kept the same as the previous study [16].  
 455 For the rigid rotational registration, the number of circumfer-  
 456 ential rays for each frame  $\gamma$  was set to 30. For the non-rigid  
 457 registration, the gradient descent-based optimization procedure  
 458 was implemented in PyTorch with the Adam optimizer [34]  
 459 with the default hyper-parameters. The parameters optimized  
 460 were the relative stretch vector  $\mathbf{x}^s$ , the relative twist vector  
 461  $\mathbf{x}^\theta$ , and the control points associated with the transverse dis-  
 462 placements  $\mathbf{p}^{d,u}$ , and  $\mathbf{p}^{d,v}$ . A learning rate of 0.001 was used  
 463 for the non-rigid longitudinal parameters while the non-rigid  
 464 rotational and non-rigid transverse parameters had a learning  
 465 rate of 0.01. This was done to encourage rough longitudinal  
 466 alignment of bifurcations early in the optimization process.  
 467 Each co-registration procedure was run for a minimum of 200  
 468 iterations to ensure convergence. The number of control points  
 469  $m_s$ ,  $m_\theta$ , and  $m_d$  were chosen to be 30, 20, and 60 respectively,  
 470 to match the frequency of variation for each aspect of catheter  
 471 motion. The relative deformation of the longitudinal control  
 472 points  $\mathbf{p}_s$  was limited to be 0.35 times the inter-point distance.  
 473 Finally, the Gaussian kernel used to smooth the SDFs was  
 474 implemented with a standard deviation of 0.1 and a kernel  
 475 size of three voxels.

476 *4) Baseline approach:* The most commonly used automatic  
 477 co-registration methodologies employed for coronary artery  
 478 registration have been discrete optimization approaches such  
 479 as DTW and DP. In order to evaluate the performance  
 480 of our longitudinal and rotational co-registration framework  
 481 against state-of-the-art discrete approaches, we applied the  
 482 methodology described in our previous work by Karmakar  
 483 et. al [18] on the same dataset. The approach utilizes DTW  
 484 to longitudinally align two coronary imaging modalities and  
 485 DP to rotationally align each frame. We utilized a window  
 486 length of four frames and recorded identical alignment metrics  
 487 for 114 matched bifurcations in the dataset. The non-rigid  
 488 registration algorithm was applied after our rigid longitudinal  
 489 registration step described in section II-A.3.

490 *5) Vessel wall segmentation model:* In this study, our rigid  
 491 rotational registration procedure required approximate vessel  
 492 wall segmentations. As the rotational registration initialization  
 493 was only required to be approximate, the segmentations were  
 494 not required to be high-fidelity or topologically accurate.  
 495 Therefore, a segmentation network was trained to produce  
 496 vessel wall label maps from 2D intravascular OCT frames. We  
 497 utilized a U-net architecture with a resnet50 encoder [35]. Our  
 498 dataset consisted of a mixture between a previously annotated  
 499 dataset [36] consisting of 8 OCT pullbacks and two newly  
 500 annotated OCT pullbacks from the P3 trial dataset, totaling  
 501 1500 2D OCT frames. 105 frames corresponding to one entire

502 pullback were held out for validation. For augmentation, we  
 503 utilized random affine transformations with a rotational range  
 504 of  $[0, 180]$  degrees and a scale range of  $[0.6, 1.4]$ . A learning  
 505 rate of 0.0001 was used in tandem with the Adam optimizer.  
 506 When applied to the validation set, the model exhibited a  
 507 precision of 0.85 and a binary dice score of 0.78.

### 508 III. RESULTS

#### 509 A. Longitudinal registration

510 Longitudinal registration can be qualitatively seen in Fig. 4,  
 511 where the non-rigid registration process aligned the majority  
 512 of common bifurcations in both imaging modalities. The  
 513 improvements over rigid registration are further visualized  
 514 by a longitudinal mismatch plot (Fig. 5A), revealing that  
 515 after rigid alignment, the percentage of bifurcations matched  
 516 within two, four, and six frames are 26.3, 42.1, and 57.9%,  
 517 respectively, while after non-rigid alignment, these values  
 518 increase to 60.5, 78.9, and 86.8%. Examining the mismatch  
 519 distribution through the longitudinal mismatch violin plot in  
 520 Fig. 6, it can be shown that using rigid registration alone, there  
 521 exists a significant variability in longitudinal mismatch, with  
 522 the median mismatch being six frames. However, after non-  
 523 rigid alignment (Fig. 6), distinct improvement can be observed  
 524 with a majority of bifurcations experiencing a decrease in  
 525 longitudinal mismatch, with the median mismatch decreasing  
 526 to 2 frames. Table I further demonstrates the effect of non-  
 527 rigid registration, in which the mean frame difference after  
 528 rigid registration was 7.9 frames (1.58 mm) and subsequently  
 529 decreased to 3.3 frames (0.66 mm) after non-rigid registration.  
 530 Statistical significance between the longitudinal non-rigid and  
 531 rigid registration error was determined by a Wilcoxon signed  
 532 rank test ( $p < 0.001$ ).

#### 533 B. Rotational registration

534 Examination of the individual bifurcating frames in Fig. 4  
 535 for the CCTA (row 1) and OCT (row 2) frames indicates  
 536 qualitative rotational and transverse alignment between both  
 537 imaging modalities as evident from the raw images and the  
 538 overlapped segmentations (row 3). Furthermore, Fig. 7 demon-  
 539 strates co-registration of calcific inclusions in regions adjacent  
 540 to properly aligned bifurcations. Rotational registration plots  
 541 in Fig. 6 quantitatively demonstrate that many bifurcations  
 542 exhibit high levels of angular misalignment, with a median  
 543 misalignment of 25.8 degrees. After non-rigid alignment, a  
 544 significant number of misaligned bifurcations were enhanced  
 545 in terms of their alignment, bringing the median mismatch  
 546 down to 8.8 degrees. Examination of the rotational mismatch  
 547 plot (Fig. 5) quantitatively demonstrates an increase in the  
 548 percentage of bifurcations aligned up to an angular mismatch  
 549 of 10, 20, and 30 degrees from % values of 25.3, 40.4, and  
 550 52.3 to 51.5, 69.7, and 79.8%, respectively. The mean value  
 551 of the angular mismatch before and after non-rigid alignment  
 552 is reported in Table I, in which the mean angular mismatch  
 553 decreases from 36.0 to 28.6 degrees. Statistical significance  
 554 between the rotational non-rigid and rigid registration error  
 555 was determined by a Wilcoxon signed rank test ( $p < 0.001$ ).

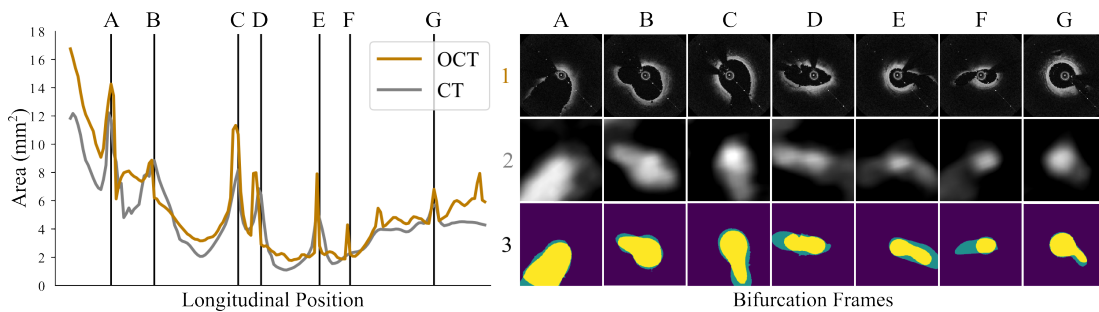


Fig. 4. Qualitative results for a single co-registered case. The left plot displays the area along the artery for the non-rigidly registered CCTA (gray) and the OCT images (gold). The right plot displays the bifurcation zones (Sections A-G) that are marked and labeled for further visualization. Bifurcation frames from the CT, OCT, and overlapped segmentation maps are presented in the first, second, and third row for qualitative comparison.

### C. Comparison with baseline

A direct comparison of our virtual catheter method with state-of-the-art discrete optimization approaches can be seen in Table I. Comparing the virtual catheter method to a discrete optimization approach for longitudinal registration, it can be seen that DTW produces significantly poorer results in longitudinal registration, with the longitudinal mismatch of 11.7 frames (2.34 mm) being higher than rigid longitudinal registration average of 7.9 frames. Comparing the virtual catheter method to using DP for rotational registration, discrete optimization algorithms exhibit poor performance for CT-OCT rotational registration (angular mismatch of 77.9 degrees) which is higher than the angular mismatch after rigid rotational registration alone. Statistical significance between registration errors was determined by a Wilcoxon signed rank test ( $p < 0.001$ ).

TABLE I

ACCURACY OF CO-REGISTRATION APPROACHES APPLIED TO CT-OCT IMAGE REGISTRATION. AVERAGE ERRORS AND STANDARD DEVIATIONS IN LONGITUDINAL (FRAMES) AND ROTATIONAL (DEGREE) DIRECTIONS. ALL APPROACHES IN CT-OCT ARE EVALUATED ON THE SAME DATASET

Method	Modalities	Subjects	Frame mismatch	Degree mismatch
[18]	OCT-OCT	9	$0.9 \pm 0.8$	$7.7 \pm 6.7$
[37]	OCT-OCT	21	$5.6 \pm 6.7$	$1.2 \pm 0.81$
[18]	OCT-IVUS	7	$1.45 \pm 0.7$	$29.1 \pm 23.2$
[15]	OCT-IVUS	12	$5.0 \pm 6.2$	$17.8 \pm 21.9$
[18]	CT-OCT	40	$11.7 \pm 12.1$	$77.9 \pm 61.0$
Ours (Rigid)	CT-OCT	40	$7.9 \pm 7.1$	$36.0 \pm 31.9$
Ours (Non-rigid)	CT-OCT	40	$3.3 \pm 3.9$	$28.6 \pm 40.9$

## IV. DISCUSSION

The aim of the current study was to develop a semi-automatic registration algorithm to align CCTA and intravascular images given the equivalent vessel morphology and a CCTA centerline as guiding inputs. Specifically, we propose a novel registration process that involves finding the optimal rigid and non-rigid spatial transforms applied to a virtual catheter moving through the CCTA image, aligning both modalities. Our results indicate that our co-registration methodology can align CCTA and OCT frames with a high degree of fidelity, as evidenced by the alignment of reference landmark annotations (Fig. 4). Further, our results underline

the critical importance of a non-rigid registration step, with significant enhancement in both longitudinal and rotational alignments as seen when comparing rigid vs. non-rigid alignments in Table I. We demonstrate that for the majority of bifurcations, our framework is able to improve the longitudinal and rotational alignment of common bifurcations within the CCTA and OCT images (Fig. 6). Lastly, we demonstrate the added value of our approach as compared to state-of-the-art alternatives, with a head-to-head comparison to previously developed discrete optimization alignment algorithms (Table I). This comparison demonstrates that discrete optimization approaches for longitudinal and rotational alignment suffer a significant drop in alignment quality when applied for the task of CT-OCT co-registration. Meanwhile, our approach maintains performance metrics in line with intravascular-intravascular image registration.

### A. Related work

Currently, a majority of CCTA studies that validate their findings with intravascular images have used manual registration based on fiduciary landmarks such as bifurcations or large calcifications [1], [38]–[40]. In comparison, our approach implicitly matches nearby bifurcations using morphological representations of the CCTA and OCT lumen. Other approaches that automatically register intravascular-to-intravascular modalities have in the past relied on DTW [15], [18], to maximize longitudinal and rotational alignment of separate intravascular pullbacks.

Direct numerical comparison of reported co-registration accuracy across published approaches is inherently difficult as co-registration accuracy is highly dependent on the specific datasets used as well as which modalities are being co-registered. For example, co-registration accuracy is higher for single-modality datasets (OCT-OCT) compared to datasets that include multiple modalities (OCT-IVUS) (Table I). Moreover, this problem is made more difficult as many co-registration studies are conducted on small and private datasets consisting of few patients. In contrast, we leverage a multi-center dataset of 40 patients that is significantly larger than the average dataset size of comparable prior studies. We also directly compare with our previously developed discrete optimization algorithm [18] to control for dataset variability, finding that our prior work produced significantly worse longitudinal and



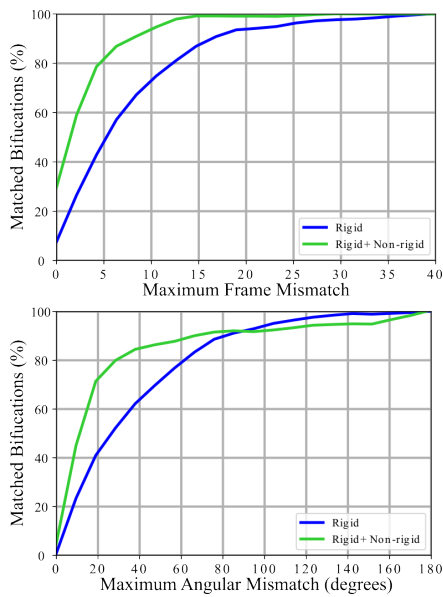


Fig. 5. Quantitative results comparing rigid and non-rigid co-registration in longitudinal and rotational directions with varying degrees of misalignment. Mismatch plots exhibit the % of matched bifurcations with increasing longitudinal (top) and rotational (bottom) alignment mismatch criteria (x-axis).

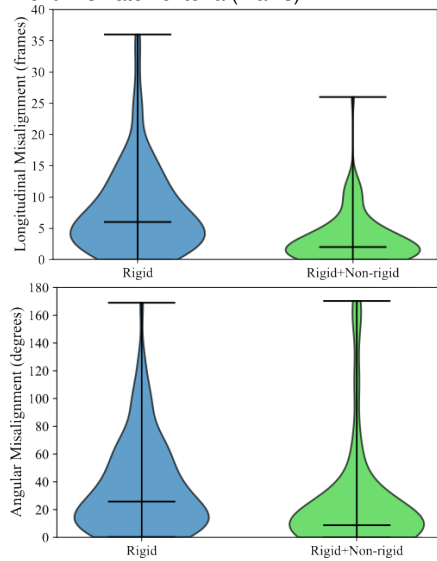


Fig. 6. Violin plots comparing rigid and non-rigid co-registration in longitudinal and rotational directions. Horizontal bars mark median and extremes. First row compares longitudinal bifurcation frame mismatch before and after non-rigid registration. Second row compares bifurcation angular mismatch before and after non-rigid registration. Bifurcations that were longitudinally matched within six OCT frames after non-rigid registration were plotted in the second row.

igate such challenges. First, the comparatively low resolution of CCTA images induces a circular bias in the already circular lumen segmentations (see Fig. 4), as well as a tendency to miss small bifurcations. Such circularly symmetric regions create zones of longitudinal and rotational ambiguity along the pull-back. Our approach minimizes this effect by formulating the longitudinal and rotational transforms in terms of regularized and smooth B spline deformations. As such, the optimization procedure is mainly guided by the alignment of prominent non-symmetric features such as bifurcations, rather than the circularly symmetric lumen segments. This incentivizes the rotational alignment of all non-bifurcating lumen frames that are in proximity to their matched bifurcations (Fig. 4).

Another significant issue faced in previous rotational co-registration algorithms [15], [18] is that lumen bifurcations are only able to contribute to rotational alignment if they exist within the same frame. As such, poor longitudinal alignment of bifurcations was a significant contributing factor to the poor performance of our previously developed DP algorithm for rotational co-registration (Table I). Our current framework, in contrast, minimizes this dependency through the use of a 1D Gaussian smoothing kernel applied longitudinally over the OCT morphology. Longitudinal smoothing allows single-frame bifurcations to appear in adjacent frames and smooths the loss surface such that bifurcations in the different modalities can be better aligned (Fig. 4).

Lastly, many co-registration methods normalize the position of the lumen by the artery centroid [1], [15], [16], [18]. While such an approach manages to align CCTA and OCT frames with circularly symmetric lumens, it fails to align equivalent frames with bifurcations, due to differing centroids between the modalities. Moreover, centering the image around the lumen centroids can cause the algorithm to mistakenly align bifurcations 180-degrees from the correct orientation. In our current framework, we instead choose to jointly optimize for the transverse displacements of the catheter path frames in addition to the longitudinal and rotational displacements, which allows for the bifurcations in both modalities to be anchored around the OCT catheter location and enables near pixelwise alignment of the lumen (Fig. 4) and plaque constituents such as calcium (Fig. 7).

In contrast to approaches that minimize image similarity for co-registration [41], our morphology-based approach is agnostic to the specific intravascular imaging modality provided that luminal segmentations are available. As such, it is likely that our non-rigid algorithm can be readily extended to co-register CCTA and IVUS images, as IVUS can visualize the lumen with similar quality compared to OCT images, albeit with a minor bias towards over-estimating the lumen area [42], [43]. However, the applicability of rigid rotational registration with IVUS-derived vessel wall segmentations is an open question. On one hand, calcified plaque can significantly effect the visualization of the wall through acoustic shadowing [43] which can impact the rotational registration accuracy after rigid registration. On the other hand, rigid rotational registration must only produce an adequate initialization for the non-rigid registration algorithm, which may be insensitive to non-extensive imaging artifacts. Moreover, rigid registration

rotational alignment compared to the virtual catheter method for the case of CT-OCT registration (Table I). In contrast, our developed methodology achieves similar results to studies involving intravascular-intravascular registration (Table I).

### B. Methodological adaptations

The task of co-registering CCTA and OCT images presents several unique difficulties for discrete registration algorithms. Our framework has several features that were designed to mit-

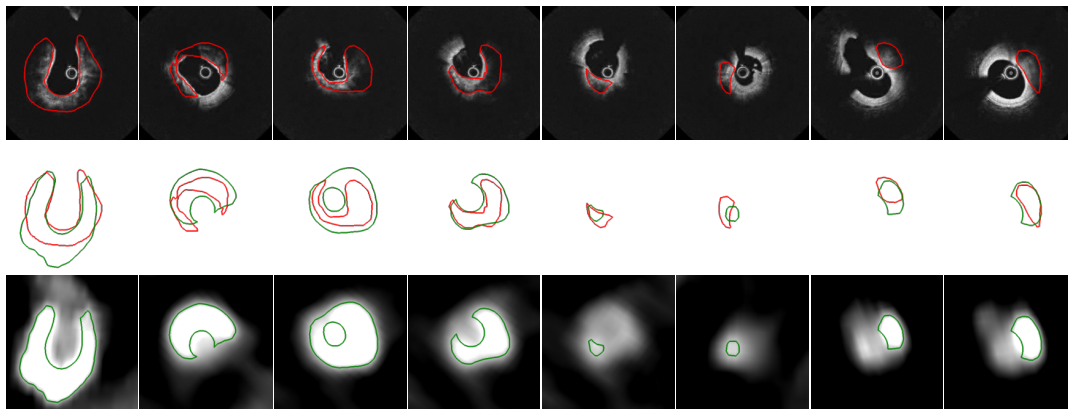


Fig. 7. Qualitative results comparing calcium annotations between CCTA (first row, obtained by thresholding) and OCT (third row, obtained by manual annotation) for selected frames with sufficient luminal alignment. Middle row shows superimposed calcium annotations for OCT (red) and CCTA (green).

692 can be approximated with the annotation of a single fiduciary  
693 landmark, meaning that our non-rigid algorithm can nonethe-  
694 less accelerate registration without relying on IVUS-derived  
695 vessel wall segmentations.

### 696 C. Limitations

697 Though very promising for clinical applications, our de-  
698 veloped approach has a number of limitations. First, the  
699 non-rigid spatial transform acting on the virtual catheter is  
700 found through gradient-based optimization, requiring that the  
701 rigid initialization brings landmarks sufficiently close such  
702 that proper matching is ensured. For example, common bi-  
703 furcations that have a frame mismatch of more than six  
704 frames (corresponding to the longitudinal smoothing kernel)  
705 are expected to be uncorrelated in terms of orientation. This  
706 issue can be mitigated by training a neural network to predict  
707 the spatial transform needed to align the two modalities. As  
708 our developed spatial transforms are differentiable, they can  
709 be integrated into deep learning workflows with relative ease.  
710 Another limitation is the dependence of non-rigid registration  
711 on the lumen segmentations. The lumen estimation for bifur-  
712 cations is expected to be accurate for both modalities and  
713 as such, ensures good registration accuracy for regions that  
714 include many such landmarks. However, due to the low reso-  
715 lution of CCTA as compared to intravascular modalities, the  
716 lumen estimation tends to be highly circular in vessel sections  
717 without bifurcations. Accordingly, it is expected that rotational  
718 co-registration certainty increases with bifurcation proximity  
719 but decreases in regions that contain highly circular luminal  
720 profiles. In the future, co-registration accuracy can likely be  
721 improved by including contextual information relating to the  
722 vessel wall such as lesion morphology as a supervisory signal  
723 in the loss function. Furthermore, the use of a pixel-wise loss  
724 as a surrogate for luminal alignment may not necessarily result  
725 in optimal alignment of lumen bifurcations. In the future, this  
726 issue can be mitigated by introducing an orientation loss to  
727 bias the spatial transform to rotationally align bifurcations.  
728 Lastly, regularizing the spatial transform and smoothing the  
729 SDFs can create difficulties in localizing landmarks up to

frame-wise precision. This can be seen in the area curve 730  
in Fig. 4 section B with the slightly mismatched bifurcation 731  
in the longitudinal direction. The localization capabilities of 732  
the algorithm can be improved by introducing multi-scale 733  
deformation steps where finer control point grids can be 734  
recursively used as the basis for the spatial transform. 735

### V. CONCLUSION

736 We present a semi-automatic algorithm for the co- 737  
registration of CCTA and intravascular images. We formulate 738  
rigid and non-rigid registration algorithms to reconstruct the 739  
3D path of the intravascular catheter, enabling a frame-to- 740  
frame comparison between modalities. Specifically, we use 741  
automatic differentiation to optimize for the virtual catheter 742  
path throughout the CCTA-derived lumen that recapitulates 743  
the lumen morphology as found in the intravascular image. 744  
Key to our approach is a differentiable spatial transform that 745  
models the non-rigid motion of the virtual catheter in the 746  
longitudinal, rotational, and transverse directions. Our non- 747  
rigid registration algorithm enables the creation of matched 748  
multi-modal datasets for various clinical applications and can 749  
be used in machine learning-based frameworks. 750

### REFERENCES

- 751
- 752 [1] K. Uzu, H. Otake, G. Choi, T. Toba, H. J. Kim, A. Roy, M. Schaap,  
753 L. Grady, M. Kawata, T. Shinke *et al.*, "Lumen boundaries extracted  
754 from coronary computed tomography angiography on computed  
755 fractional flow reserve (ffrct): validation with optical coherence tomog-  
756 raphy." *Eurointervention: Journal of Europr in Collaboration with the  
757 Working Group on Interventional Cardiology of the European Society  
758 of Cardiology*, vol. 14, no. 15, pp. e1609–e1618, 2019.
  - 759 [2] C. Kim, S.-J. Hong, D.-H. Shin, J.-S. Kim, B.-K. Kim, Y.-G. Ko,  
760 D. Choi, Y. Jang, and M.-K. Hong, "Limitations of coronary computed  
761 tomographic angiography for delineating the lumen and vessel contours  
762 of coronary arteries in patients with stable angina," *European Heart  
763 Journal-Cardiovascular Imaging*, vol. 16, no. 12, pp. 1358–1365, 2015.
  - 764 [3] M. J. Budoff, D. Dowe, J. G. Jollis, M. Gitter, J. Sutherland, E. Halamert,  
765 M. Scherer, R. Bellinger, A. Martin, R. Benton *et al.*, "Diagnostic  
766 performance of 64-multidetector row coronary computed tomographic  
767 angiography for evaluation of coronary artery stenosis in individuals  
768 without known coronary artery disease: results from the prospective  
769 multicenter accuracy (assessment by coronary computed tomographic  
770 angiography of individuals undergoing invasive coronary angiography)

- trial,” *Journal of the American College of Cardiology*, vol. 52, no. 21, pp. 1724–1732, 2008.
- [4] Y. Takahashi, T. Toba, H. Otake, Y. Fukuyama, S. Nakano, Y. Matsuoka, K. Tanimura, Y. Izawa, H. Kawamori, A. K. Kono *et al.*, “Feasibility of morphological assessment of coronary artery calcification with electrocardiography-gated non-contrast computed tomography: a comparative study with optical coherence tomography,” *The International Journal of Cardiovascular Imaging*, vol. 37, no. 4, pp. 1445–1453, 2021.
- [5] C. Fischer, E. Hulten, P. Belur, R. Smith, S. Voros, and T. C. Villines, “Coronary ct angiography versus intravascular ultrasound for estimation of coronary stenosis and atherosclerotic plaque burden: a meta-analysis,” *Journal of cardiovascular computed tomography*, vol. 7, no. 4, pp. 256–266, 2013.
- [6] M. A. De Graaf, A. Broersen, P. H. Kitslaar, C. J. Roos, J. Dijkstra, B. P. Lelieveldt, J. W. Jukema, M. J. Schalij, V. Delgado, J. J. Bax *et al.*, “Automatic quantification and characterization of coronary atherosclerosis with computed tomography coronary angiography: cross-correlation with intravascular ultrasound virtual histology,” *The international journal of cardiovascular imaging*, vol. 29, no. 5, pp. 1177–1190, 2013.
- [7] H. Brodoefel, C. Burgstahler, M. Heuschmid, A. Reimann, F. Khosa, A. Kopp, S. Schroeder, C. Claussen, and M. Clouse, “Accuracy of dual-source ct in the characterisation of non-calcified plaque: use of a colour-coded analysis compared with virtual histology intravascular ultrasound,” *The British journal of radiology*, vol. 82, no. 982, pp. 805–812, 2009.
- [8] K. Kadry, M. L. Olender, D. Marlevi, E. R. Edelman, and F. R. Nezami, “A platform for high-fidelity patient-specific structural modelling of atherosclerotic arteries: from intravascular imaging to three-dimensional stress distributions,” *Journal of the Royal Society Interface*, vol. 18, no. 182, p. 20210436, 2021.
- [9] R. Straughan, K. Kadry, S. A. Parikh, E. R. Edelman, and F. R. Nezami, “Fully automated construction of three-dimensional finite element simulations from optical coherence tomography,” *Computers in Biology and Medicine*, vol. 165, p. 107341, 2023.
- [10] M. van Assen, A. Varga-Szemes, U. J. Schoepf, T. M. Duguay, H. T. Hudson, S. Egorova, K. Johnson, S. S. Pierre, B. Zaki, M. Oudkerk *et al.*, “Automated plaque analysis for the prognostication of major adverse cardiac events,” *European Journal of Radiology*, vol. 116, pp. 76–83, 2019.
- [11] G. Poletti, L. Antonini, L. Mandelli, P. Tsompou, G. S. Karanasiou, M. I. Papafaklis, L. K. Michalis, D. I. Fotiadis, L. Petrini, and G. Pennati, “Towards a digital twin of coronary stenting: a suitable and validated image-based approach for mimicking patient-specific coronary arteries,” *Electronics*, vol. 11, no. 3, p. 502, 2022.
- [12] F. Rikhtegar, E. R. Edelman, U. Olgac, D. Poulidakos, and V. Kurtcuoglu, “Drug deposition in coronary arteries with overlapping drug-eluting stents,” *Journal of Controlled Release*, vol. 238, pp. 1–9, 2016.
- [13] N. Tsiknakis, C. Spanakis, P. Tsompou, G. Karanasiou, G. Karanasiou, A. Sakellarios, G. Rigas, S. Kyriakidis, M. Papafaklis, S. Nikopoulos *et al.*, “Ivus longitudinal and axial registration for atherosclerosis progression evaluation,” *Diagnostics*, vol. 11, no. 8, p. 1513, 2021.
- [14] H. Qin, C. Li, Y. Li, J. Huang, F. Yang, T. Kubo, T. Akasaka, C. Xiao, J. L. Gutiérrez-Chico, and S. Tu, “Automatic coregistration between coronary angiography and intravascular optical coherence tomography: Feasibility and accuracy,” *JACC: Asia*, vol. 1, no. 2, pp. 274–278, 2021.
- [15] D. S. Molony, L. H. Timmins, E. Rasoul-Arzumly, H. Samady, and D. P. Giddens, “Evaluation of a framework for the co-registration of intravascular ultrasound and optical coherence tomography coronary artery pullbacks,” *Journal of biomechanics*, vol. 49, no. 16, pp. 4048–4056, 2016.
- [16] A. Karmakar, M. L. Olender, F. R. Nezami, D. Marlevi, E. Shlofmitz, R. A. Shlofmitz, and E. R. Edelman, “Detailed investigation of lumen-based tomographic co-registration,” in *2020 IEEE International Conference on Bioinformatics and Biomedicine (BIBM)*. IEEE, 2020, pp. 1038–1042.
- [17] Y. Gharaibeh, J. Lee, D. Prabhu, P. Dong, V. N. Zimin, L. A. Dallen, H. Bezerra, L. Gu, and D. Wilson, “Co-registration of pre-and post-stent intravascular oct images for validation of finite element model simulation of stent expansion,” in *Medical Imaging 2020: Biomedical Applications in Molecular, Structural, and Functional Imaging*, vol. 11317. SPIE, 2020, pp. 306–316.
- [18] A. Karmakar, M. L. Olender, D. Marlevi, E. Shlofmitz, R. A. Shlofmitz, E. R. Edelman, and F. R. Nezami, “Framework for lumen-based nonrigid tomographic coregistration of intravascular images,” *Journal of Medical Imaging*, vol. 9, no. 4, p. 044006, 2022.
- [19] L. Zhang, R. Downe, Z. Chen, S. Sun, T. Masiarov, T. Kovarnik, J. Lopez, M. Sonka, and A. Wahle, “Side-branch guided registration of intravascular ultrasound pullbacks in coronary arteries,” in *MICCAI Workshop in Computing and Visualization for IntraVascular Imaging and Computer Assisted Stenting (CVII-STENT)*, 2014, pp. 44–51.
- [20] G. Balakrishnan, A. Zhao, M. R. Sabuncu, J. Guttag, and A. V. Dalca, “Voxelmorph: a learning framework for deformable medical image registration,” *IEEE transactions on medical imaging*, vol. 38, no. 8, pp. 1788–1800, 2019.
- [21] Y. Fu, Y. Lei, T. Wang, W. J. Curran, T. Liu, and X. Yang, “Deep learning in medical image registration: a review,” *Physics in Medicine & Biology*, vol. 65, no. 20, p. 20TR01, 2020.
- [22] V. Gopalakrishnan, N. Dey, and P. Golland, “Intraoperative 2d/3d image registration via differentiable x-ray rendering,” *arXiv preprint arXiv:2312.06358*, 2023.
- [23] M. Jaderberg, K. Simonyan, A. Zisserman *et al.*, “Spatial transformer networks,” *Advances in neural information processing systems*, vol. 28, 2015.
- [24] V. Gopalakrishnan and P. Golland, “Fast auto-differentiable digitally reconstructed radiographs for solving inverse problems in intraoperative imaging,” in *Workshop on Clinical Image-Based Procedures*. Springer, 2022, pp. 1–11.
- [25] A. Kanitsar, D. Fleischmann, R. Wegenkittl, P. Felkel, and E. Groller, *CPR-curved planar reformation*. IEEE, 2002.
- [26] J. Guo, S. Li, Y. P. Chui, J. Qin, and P. A. Heng, “Mesh quality oriented 3d geometric vascular modeling based on parallel transport frame,” *Computers in Biology and Medicine*, vol. 43, no. 7, pp. 879–888, 2013.
- [27] T. Rohlfing, “Image similarity and tissue overlaps as surrogates for image registration accuracy: widely used but unreliable,” *IEEE transactions on medical imaging*, vol. 31, no. 2, pp. 153–163, 2011.
- [28] D. Rueckert, L. I. Sonoda, C. Hayes, D. L. Hill, M. O. Leach, and D. J. Hawkes, “Nonrigid registration using free-form deformations: application to breast mr images,” *IEEE transactions on medical imaging*, vol. 18, no. 8, pp. 712–721, 1999.
- [29] S. Nagumo, C. Collet, B. L. Norgaard, H. Otake, B. Ko, B.-k. Koo, J. Leipsic, D. Andreini, W. Heggermont, J. M. Jensen *et al.*, “Rationale and design of the precise percutaneous coronary intervention plan (p3) study: Prospective evaluation of a virtual computed tomography-based percutaneous intervention planner,” *Clinical cardiology*, vol. 44, no. 4, pp. 446–454, 2021.
- [30] O. Ronneberger, P. Fischer, and T. Brox, “U-net: Convolutional networks for biomedical image segmentation,” in *International Conference on Medical image computing and computer-assisted intervention*. Springer, 2015, pp. 234–241.
- [31] E. Treister and E. Haber, “A fast marching algorithm for the factored eikonal equation,” *Journal of Computational physics*, vol. 324, pp. 210–225, 2016.
- [32] J. Sonck, S. Nagumo, B. L. Norgaard, H. Otake, B. Ko, J. Zhang, T. Mizukami, M. Maeng, D. Andreini, Y. Takahashi *et al.*, “Clinical validation of a virtual planner for coronary interventions based on coronary ct angiography,” *Cardiovascular Imaging*, vol. 15, no. 7, pp. 1242–1255, 2022.
- [33] L. Antiga, M. Piccinelli, L. Botti, B. Ene-Iordache, A. Remuzzi, and D. A. Steinman, “An image-based modeling framework for patient-specific computational hemodynamics,” *Medical & biological engineering & computing*, vol. 46, no. 11, pp. 1097–1112, 2008.
- [34] D. P. Kingma and J. Ba, “Adam: A method for stochastic optimization,” *arXiv preprint arXiv:1412.6980*, 2014.
- [35] K. He, X. Zhang, S. Ren, and J. Sun, “Deep residual learning for image recognition. arxiv 2015,” *arXiv preprint arXiv:1512.03385*, vol. 14, 2015.
- [36] M. L. Olender, L. S. Athanasiou, M. José, E. Ben-Assa, F. R. Nezami, and E. R. Edelman, “A mechanical approach for smooth surface fitting to delineate vessel walls in optical coherence tomography images,” *IEEE transactions on medical imaging*, vol. 38, no. 6, pp. 1384–1397, 2018.
- [37] N. Tsiknakis, C. Spanakis, P. Tsoumpou, G. Karanasiou, G. Karanasiou, A. Sakellarios, G. Rigas, S. Kyriakidis, M. I. Papafaklis, S. Nikopoulos *et al.*, “Oct sequence registration before and after percutaneous coronary intervention (stent implantation),” *Biomedical Signal Processing and Control*, vol. 79, p. 104251, 2023.
- [38] S. Carlier, R. Didday, T. Slots, P. Kayaert, J. Sonck, M. El-Mourad, N. Preumont, D. Schoors, and G. Van Camp, “A new method for real-time co-registration of 3d coronary angiography and intravascular ultrasound or optical coherence tomography,” *Cardiovascular Revascularization Medicine*, vol. 15, no. 4, pp. 226–232, 2014.

- 922 [39] S. Tu, N. R. Holm, G. Koning, Z. Huang, and J. H. Reiber, "Fusion of 3d  
923 qca and ivus/oct," *The international journal of cardiovascular imaging*,  
924 vol. 27, no. 2, pp. 197–207, 2011.
- 925 [40] L. Hebsgaard, T. M. Nielsen, S. Tu, L. R. Krusell, M. Maeng, K. T.  
926 Veien, B. Raungaard, C. J. Terkelsen, A. Kaltoft, J. H. Reiber *et al.*, "Co-  
927 registration of optical coherence tomography and x-ray angiography in  
928 percutaneous coronary intervention. the does optical coherence tomog-  
929 raphy optimize revascularization (doctor) fusion study," *International*  
930 *journal of cardiology*, vol. 182, pp. 272–278, 2015.
- 931 [41] P. Viola and W. M. Wells III, "Alignment by maximization of mutual  
932 information," *International journal of computer vision*, vol. 24, no. 2,  
933 pp. 137–154, 1997.
- 934 [42] T. Kubo, T. Akasaka, J. Shite, T. Suzuki, S. Uemura, B. Yu, K. Kozuma,  
935 H. Kitabata, T. Shinke, M. Habara *et al.*, "Oct compared with ivus in a  
936 coronary lesion assessment: the opus-class study," *JACC: Cardiovascu-*  
937 *lar Imaging*, vol. 6, no. 10, pp. 1095–1104, 2013.
- 938 [43] J. Huang, K. Ninomiya, S. Tu, S. Masuda, J. Dijkstra, M. Chu, D. Ding,  
939 S. O. Hynes, N. O'Leary, W. Wijns *et al.*, "Calcified plaque detected on  
940 oct with deep learning and cross-validated with optical and ultrasound  
941 signals: A complementary appraisal and preamble to combined ivus-oct  
942 catheter," *Frontiers in Photonics*, vol. 3, p. 1019552, 2022.